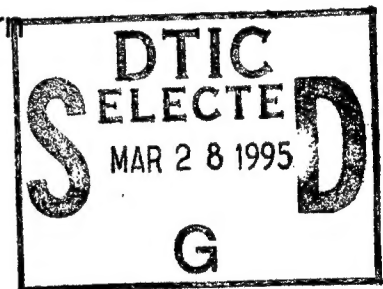


Technical Document 2734
January 1995

A Simple Method for Range Finding via Laser Triangulation

Hoa G. Nguyen
Michael R. Blackburn



19950324 058



Approved for public use; distribution is unlimited.

Technical Document 2734

January 1995

A Simple Method for Range Finding via Laser Triangulation

Hoa G. Nguyen
Michael R. Blackburn

Accession For	
NTIS	CRA&I <input checked="checked" type="checkbox"/>
DTIC	TAB <input type="checkbox"/>
Unannounced <input type="checkbox"/>	
Justification _____	
By _____	
Distribution /	
Availability Codes	
Dist	Avail and/or Special
A-1	

**NAVAL COMMAND, CONTROL AND
OCEAN SURVEILLANCE CENTER
RDT&E DIVISION
San Diego, California 92152-5001**

**K. E. EVANS, CAPT, USN
Commanding Officer**

**R. T. SHEARER
Executive Director**

ADMINISTRATIVE INFORMATION

This work was performed as part of a project funded by the Advanced Research Projects Agency and the Office of Naval Research.

Released by
D. E. Demuth, LCDR, Head
Adaptive Systems Branch

Under authority of
D. W. Murphy, Head
Advanced Systems Division

ACKNOWLEDGMENTS

The authors would like to thank Bart Everett for the use of the robot and his critiques of this report and Steve Timmer for mechanical fabrication support.

CONTENTS

INTRODUCTION	1
PROCEDURE	1
IMPLEMENTATION	3
PERFORMANCE	4
REFERENCES	5

Figures

1. Configuration for triangulation ranging.	1
2. Setup of laser and camera.	2
3. Laser and camera combination.	3
4. Robot directing remote manipulator arm.	4
5. Precision versus range.	5

INTRODUCTION

For determining range via triangulation, the baseline distance between source and sensor as well as sensor and source angles are used in theory. Figure 1 shows the configuration for triangulation ranging (Everett, 1995):

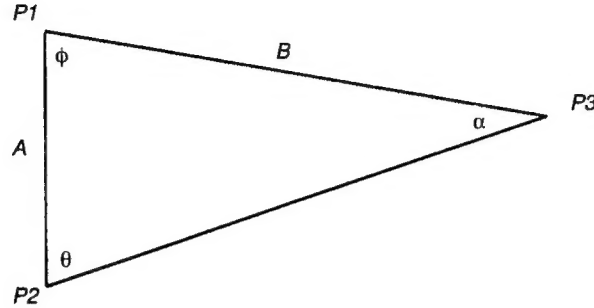


Figure 1. Configuration for triangulation ranging.

$P1$ and $P2$ represent two reference points (e.g., camera and laser source), while $P3$ is a target point. The range B can be determined from the knowledge of the baseline separation A and the angles θ and ϕ using the law of sines:

$$B = A \frac{\sin \theta}{\sin \alpha} = A \frac{\sin \theta}{\sin(\theta + \phi)} \quad (1)$$

In practice this is difficult to achieve because the baseline separation and angles are difficult to measure accurately. We have demonstrated a technique for obtaining range information via laser triangulation without the need to know A , ϕ , and θ . This technique was successfully implemented on a laser range-finding system on the NRaD ModBot (Modular Robot) test bed.

PROCEDURE

Figure 2 diagrams the setup of our laser and camera. The camera is represented by the image plane, focal point, and optical axis. The laser is directly above the camera, although its exact position is unimportant (we will only deal with the beam of light, represented by line CE in the diagram).

The laser is positioned so that the path of the laser and the optical axis form a vertical plane. Point P is the target of interest. We wish to find x , the projection of point P on the optical axis. u is the (vertical) projection of point P on the image plane (the scan line in the image on which the spot is detected). P_1 and P_2 are two points used in the calibration of the system; x_1 , x_2 , u_1 , and u_2 are known.

E is the point where the path of the laser intersects the optical axis. We angle the laser such that point E is at the center of the range of interests. However, this technique also works with the laser path parallel to the optical axis. There is no particular need for accurate determination or setting of the axes, beyond a concern for precision to be discussed later. There is also no need to know the baseline distance between camera and laser, nor the focal length (f) of the camera.

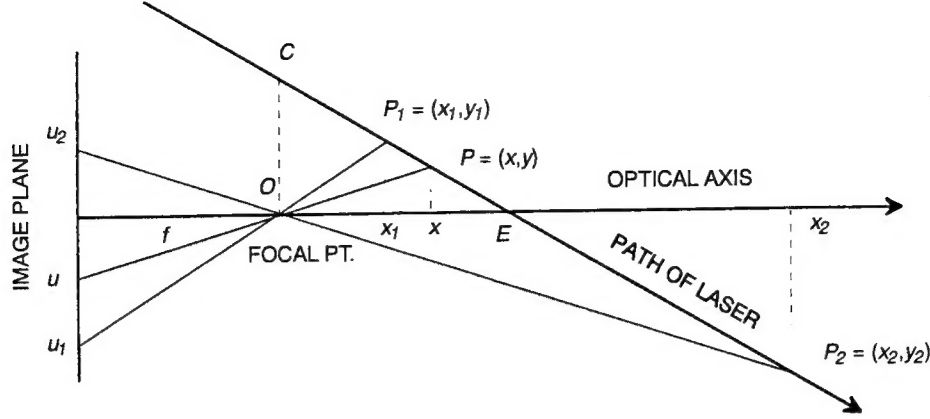


Figure 2. Setup of laser and camera.

Determination of x is achieved as follows:

From the geometry of similar triangles, we have

$$\frac{y_1}{x_1} = \frac{u_1}{f} \quad \text{and} \quad \frac{y_2}{x_2} = \frac{u_2}{f} \quad (2)$$

We place the origin of the coordinate system at the focal point, without loss of generality. The slope (m) of the laser path and the y -intercept (c , the height of point C) are:

$$m = \frac{y_2 - y_1}{x_2 - x_1} \quad \text{and} \quad c = y_2 - mx_2 \quad (3)$$

Substituting equation 2 into equation 3 to eliminate y_1 and y_2 , we have:

$$m = \frac{u_2 x_2 - u_1 x_1}{f(x_2 - x_1)} \quad \text{and} \quad c = \frac{u_2 x_2}{f} - mx_2 \quad (4)$$

We note that it is difficult to find the exact "focal point" of a given camera. However, point C in figure 2, which is directly above this focal point, can be found given measurements of y_1 and y_2 (equation 3) or knowledge of the focal length, f , (equation 4). This point can be used as the location of a "virtual" laser source, and the length OC becomes the "virtual" baseline distance. We can then proceed with the law of sines approach for range determination using these parameters.

However, f is hard to determine accurately for some lenses (e.g., zoom lenses), and y_1 and y_2 are also difficult to measure. They are the offsets perpendicular to the optical axis, not the height from the ground. Also, the optical axis does not necessarily pass through the center of the image, but varies from camera to camera.

We used a simpler method that does not require the knowledge of y_1 , y_2 , or f . We note that the line uP passing through O is represented by:

$$y = \frac{u}{f}x \quad (5)$$

and the laser path is of the form:

$$y = mx + c \quad (6)$$

Solving for x from equations 5 and 6, and simplifying using equation 4, we get:

$$x = \frac{N}{ud - k} \quad (7)$$

where N , d , and k are obtained after a simple calibration process, and

$$\begin{aligned}d &= x_2 - x_1 \\k &= u_2 x_2 - u_1 x_1 \\N &= (u_1 - u_2) x_1 x_2\end{aligned}\tag{8}$$

During calibration, we put targets at distances x_1 and x_2 from the camera, record the height u_1 and u_2 at which the laser spot striking the targets appear on the image, and compute d , k , and N using equation 8. Then, during range-finding operations, we simply note the height u of the laser spot in the image and use equation 7 to compute range. We can accomplish this without knowing the base-line separation or angles between the camera and laser source. Furthermore, equations 7 and 8 are insensitive to errors in the optical axis (i.e., $u' = a + u$, $u_1' = a + u_1$, $u_2' = a + u_2$ will give the same results).

IMPLEMENTATION

We used this laser triangulation technique in a project studying adaptive sensor-motor transformations (Blackburn and Nguyen, 1994). We needed depth information, but only a single video camera was available. The camera provided both visual information about the scene and the range to target via detection of the laser spot in the image. We attached a 5-mW solid-state diode laser on top of the charge-coupled device (CCD) camera, and used a red filter on the lens to increase sensitivity to the laser spot. The laser and camera combination, mounted on a pan-and-tilt unit on a mobile robot (ModBot), is shown in figure 3.

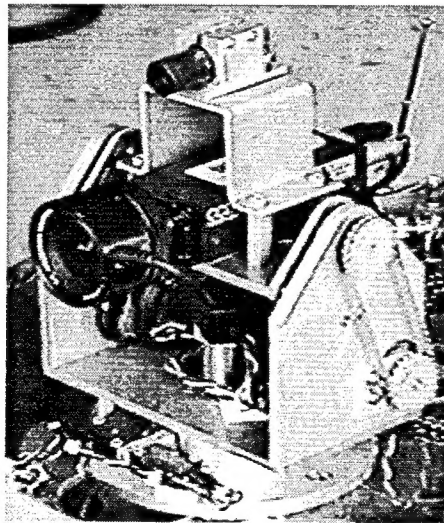


Figure 3. Laser and camera combination.

To assess target range, the target is acquired and the optical axis automatically placed at its center using the pan-and-tilt unit. The laser illuminates a spot on the target, and the vertical position of the spot in the image is used for range calculations. To accommodate small targets, the distance y (separation between laser spot and optical axis) must be kept small. This in turn means that the baseline separation between the laser source and the camera cannot be large, and the angle of the laser path must be small (fairly parallel to the optical axis). We chose to place the laser approximately 7 cm above the camera with a slight downward tilt ($E \sim 1.2$ m). The distances we were interested in were between 0.5 m and 2 m. Figure 4 shows the robot directing a remote manipulator arm to reach a cup being suspended as a target (see [Blackburn and Nguyen, 1994]).

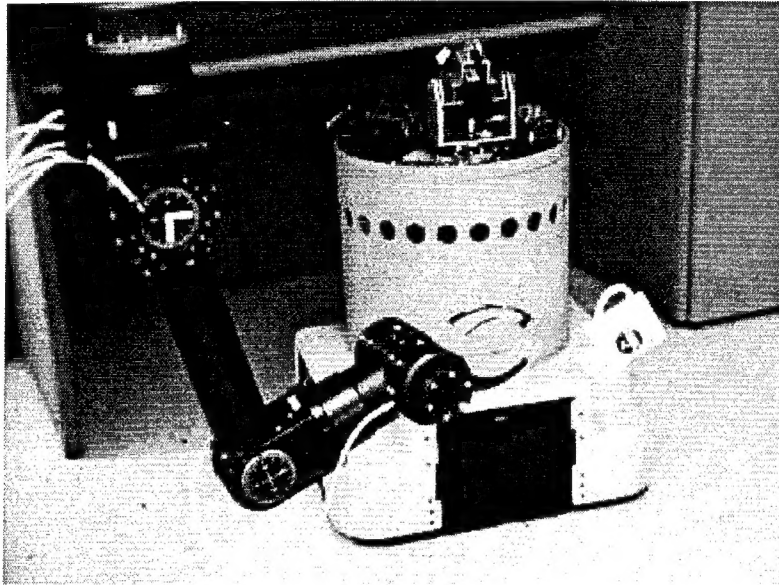


Figure 4. Robot directing remote manipulator arm.

PERFORMANCE

Our laser triangulation method is subject to a limiting factor common to all triangulation systems: reduced precision with increasing range. With the setup described above, our precision decreases from 3 mm at 30 cm to 8 cm at 1.5 m (see figure 5).

Increasing the separation distance and the laser angle will improve precision. However, in our case these are constrained by the need to keep y small. By keeping y small, we ensure that both the optical axis and the laser spot fall on the same target object (analogous to minimizing the “missing parts” problem [Everett, 1995]). Due to our somewhat unique application (i.e., motion-driven saccade mechanism), the range to target we desire is actually the distance x , and not the length OP (refer to figure 2), as is usually the case in most triangulation applications. But as a byproduct of keeping y small, $x \approx \overline{OP}$.

An alternate approach that would yield slightly higher precision is to use a lookup table that stores the predetermined range for every pixel height (see the Quantic Ranging System [Everett, 1995]). This would account for imperfections in the camera lens. But this approach is not appropriate for a research robot such as ModBot. ModBot’s laser rangefinder is used in many applications. Each

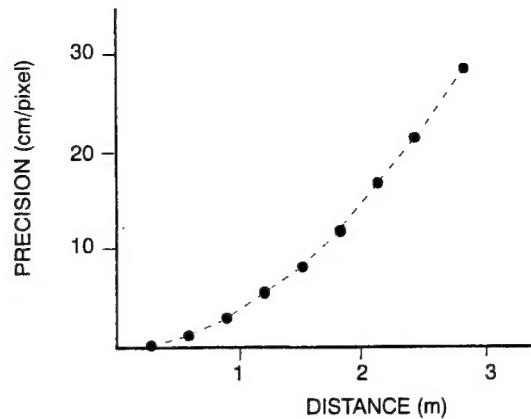


Figure 5. Precision versus range.

application requires the laser to be re-aimed to get the crossover point, E , at the middle of the range of interests (e.g., 1 m for manipulation tasks and 3 m for navigational tasks), and every change would require repeating a much more time-consuming calibration.

Another problem often associated with laser rangefinders is the specular reflections and absorption on different surfaces, decreasing detectability. We have noticed this on several instances in our application. We found that a red filter helped in the detection of the laser spot in most instances. Using a pulsed laser coupled with frame subtraction would also increase sensitivity. However, the tradeoff is that twice as many image frames would have to be digitized and transferred from the frame grabber to the processor board, and the current speed bottleneck in most real-time vision systems (including ours) is this frame-grabbing and transferring activity.

REFERENCES

1. Blackburn, Michael R., and Hoa G. Nguyen. "Robotic Sensor-Motor Transformations," *1994 Image Understanding Workshop Proc.* (pp. 209-214). November 13-16, Monterey, CA.
2. Everett, H. R. 1995 (in press). *Sensors for Mobile Robots: Theory and Application*. A K Peters, Wellesley, MA.

REPORT DOCUMENTATION PAGE

Form Approved
OMB No. 0704-0188

Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503.

1. AGENCY USE ONLY (Leave blank)		2. REPORT DATE January 1995		3. REPORT TYPE AND DATES COVERED Final	
4. TITLE AND SUBTITLE A SIMPLE METHOD FOR RANGE FINDING VIA LASER TRIANGULATION				5. FUNDING NUMBERS AN: DN301069 PE: 0601153N PROJ: MS14	
6. AUTHOR(S) Hoa G. Nguyen, Michael R. Blackburn					
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) Naval Command, Control and Ocean Surveillance Center (NCCOSC) RDT&E Division San Diego, California 92152-5000				8. PERFORMING ORGANIZATION REPORT NUMBER TD 2734	
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES) Office of Naval Research (ONR) Cognitive and Neural S&T Division 800 N. Quincy Street Arlington, VA 22217-5000 Advanced Research Projects Agency (ARPA) ATTN: SISTO 3701 N. Fairfax Dr. Arlington, VA 22203-1714				10. SPONSORING/MONITORING AGENCY REPORT NUMBER	
11. SUPPLEMENTARY NOTES					
12a. DISTRIBUTION/AVAILABILITY STATEMENT Approved for public use; distribution is unlimited.				12b. DISTRIBUTION CODE	
13. ABSTRACT (Maximum 200 words) We present the design and implementation of a simple range finder for robotic applications via laser triangulation. The technique does not require knowledge of baseline separation and angles from camera and laser to the target. The system has been successfully implemented on a mobile robot, providing range information for controlling a remote manipulator.					
14. SUBJECT TERMS laser range finding laser triangulation range finders for robotic applications				15. NUMBER OF PAGES 13	
				16. PRICE CODE	
17. SECURITY CLASSIFICATION OF REPORT UNCLASSIFIED	18. SECURITY CLASSIFICATION OF THIS PAGE UNCLASSIFIED	19. SECURITY CLASSIFICATION OF ABSTRACT UNCLASSIFIED	20. LIMITATION OF ABSTRACT SAME AS REPORT		

UNCLASSIFIED

21a. NAME OF RESPONSIBLE INDIVIDUAL Hoa G. Nguyen	21b. TELEPHONE (include Area Code) (619) 553-1871	21c. OFFICE SYMBOL Code 531

INITIAL DISTRIBUTION

Code 0012	Patent Counsel	(1)
Code 0271	Archive/Stock	(6)
Code 0274	Library	(2)
Code 50	H. O. Porter	(1)
Code 53	D. W. Murphy	(1)
Code 531	LCDR D. E. Demuth	(1)
Code 531	H. G. Nguyen	(50)
Code 531	M. R. Blackburn	(50)

Defense Technical Information Center
Alexandria, VA 22304-6145 (4)

NCCOSC Washington Liaison Office
Washington, DC 20363-5100

Center for Naval Analyses
Alexandria, VA 22302-0268

Navy Acquisition, Research and Development
Information Center (NARDIC)
Arlington, VA 22244-5114

GIDEP Operations Center
Corona, CA 91718-8000